



THE SILENT EVOLUTION

CENTAX-LFSM

SHAFT COUPLING WITH INTEGRATED THRUST BEARING – CENTAX-SEC DESIGN

ENGLISH

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CENTAX-LFSM

THE SILENT EVOLUTION

SYSTEM	TECHNICAL DATA	SERVICE
At a glance Page 03	Product application: Which feature for which coupling? Page 5	Explanation of the technical data Page APP-1
		Contact Page APP-6

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CENTAX-SEC

AT A GLANCE

CENTA offers a modular CENTAX-SEC coupling system, which allows a constructive maximum of flexibility.

The components of the series are perfectly matched: multiple combinations allow for various features, and easy control of any torsional situation. Ensuring reliable compensation of axial misalignments three optional components are available (membranes, bolts, links), emphasizing CENTA as the supplier with the most multifaceted portfolio in the market.

For efficient and fast customized solutions.

Features

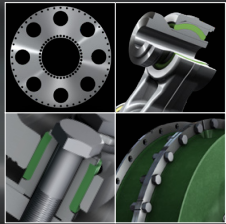
- High flexibility in design
- High flexibility in all directions
- High flexibility in torsional elasticity
- High allowable power loss

Areas of Application



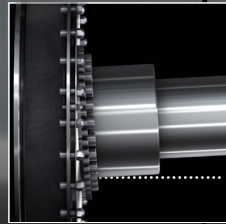
Torque range	1 to 650 kNm
Temperature range	- 45° up to + 80°C

CENTAX-LFSM SYSTEM



MODULARITY

Multiple combinations of the CENTAX-LFSM coupling programm components are available. This modularity allows for adequate design for any application. For efficient and fast customized solutions.



FUNCTIONS

The CENTAX-LFSM coupling programm offers many functions to protect your drive from harmful torsional vibrations, to compensate misalignment and to dampen vibrations and noise. Reliable power transmission for your applications with an optimum of features.



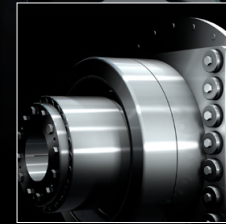
COMPENSATION OF
MISALIGNMENT

The CENTAX-LFSM rubber elements are torsionally and radially highly flexible. Combined with three optional components (membranes, links or bolts) each application gets the necessary flexibility in axial and angular direction.



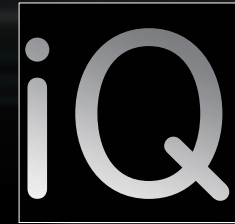
DAMPING

The torsional elasticity of each application is variably tuned by the components applied. Shocks and vibrations are dampened, resonances shifted to subcritical ranges and a very low noise level for more comfort on board is achieved.



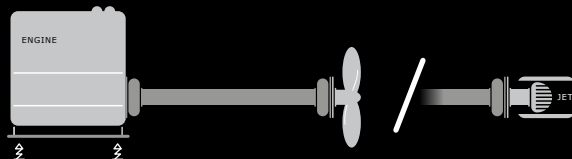
THRUST BEARING

The patented Thrust Bearing design of the CENTAX-LFSM system cuts off and damps the propeller thrust.



QUALITY

When the going get's tough, quality is priceless. With an exemplary Quality Management, CENTA ensures products that withstand the roughest assignments. CENTA's coupling systems are more than the sum of their parts. CENTA entertains the vision of intelligent products that meet the highest requirements in terms of design and quality.



EXPLANATION OF THE TECHNICAL DATA

This appendix shows all explanations of the technical data for all CENTA products.
the green marked explanations are relevant for this catalog:

1	Size	Page APP-2
2	Rubber quality	Page APP-2
3	Nominal torque	Page APP-2
4	Maximum torque	Page APP-2
5	Continuous vibratory torque	Page APP-2
6	Permissible power loss	Page APP-2
7	Dynamic torsional stiffness	Page APP-3
8	Relative damping	Page APP-3
9	Speed	Page APP-3
10	Permissible axial displacement	Page APP-3
11	Axial stiffness	Page APP-4
12	Permissible radial displacement	Page APP-4
13	Radial stiffness	Page APP-4
14	Permissible angular displacement	Page APP-4
15	Angular stiffness	Page APP-4

Are these technical explanations up to date?
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EXPLANATION OF THE TECHNICAL DATA

1

Size

This spontaneously selected figure designates the size of the coupling.

2

Rubber quality
Shore A

This figure indicates the nominal shore hardness of the elastic element.
The nominal value and the effective value may deviate within given tolerance ranges.

3

Nominal torque
 T_{KN} [kNm]

Average torque which can be transmitted continuously over the entire speed range.

4

Maximum torque
[kNm]

T_{Kmax}

This is the torque that may occur occasionally and for a short period up to 1.000 times and may not lead to a substantial temperature rise in the rubber element.

In addition the following maximum torques may occur:

$\Delta T_{Kmax} = 1,8 \times T_{KN}$

Peak torque range (peak to peak) between maximum and minimum torque, e.g. switching operation.

$T_{Kmax1} = 1,5 \times T_{KN}$

Temporary peak torque (e.g. passing through resonances). ΔT_{Kmax} or T_{Kmax1} may occur 50.000 times alternating or 100.000 times swelling.

$T_{Kmax2} = 4,5 \times T_{KN}$

Transient torque rating for very rare, extraordinary conditions (e.g. short circuits).

5

Continuous vibratory torque
 T_{KW} [kNm]

Amplitude of the continuously permissible periodic torque fluctuation with a basic load up to the value T_{KN} .
The frequency of the amplitude has no influence on the permissible continuous vibratory torque. Its main influence on the coupling temperature is taken into consideration in the calculation of the power loss.

Operating torque
 T_{Bmax} [kNm]

The maximum operating torque results of T_{KN} and T_{KW} .

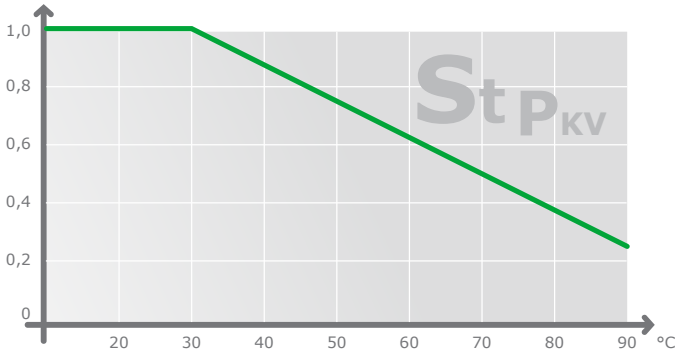
6

Permissible Power Loss
 P_{KV} [kW] or [W]

Damping of vibrations and displacement results in power loss within the rubber element.
The permissible power loss is the maximum heat (converted damping work into heat), which the rubber element can dissipate continuously to the environment (i.e. without time limit) without the maximum permissible temperature being exceeded.
The given permissible power loss refers to an ambient temperature of 30° C.
If the coupling is to be operated at a higher ambient temperature, the temperature factor S_{tPKV} has to be taken into consideration in the calculation.
The coupling can momentarily withstand an increase of the permissible power loss for a short period under certain operation modes (e.g. misfiring).

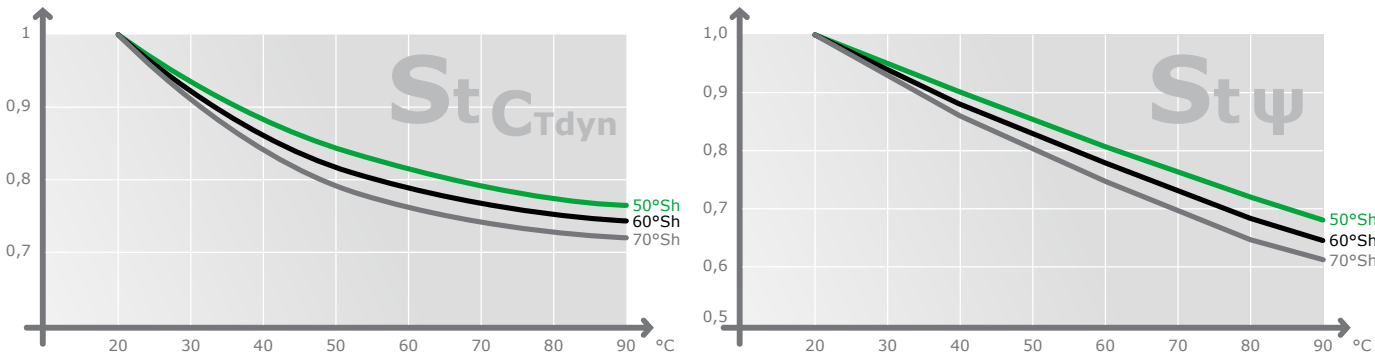
P_{KVZ} [kW]

Defines an individual and proven guide for power loss under misfiring. This value acknowledges general information of the engine suppliers, in particular the real appearance of misfiring and implemented control and protection devices. Values on request.



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EXPLANATION OF THE TECHNICAL DATA



7
Dynamic torsional stiffness
C_{Tdyn} [kNm/rad]

The dynamic torsional stiffness is the relation of the torque to the torsional angle under dynamic loading.

The torsional stiffness may be linear or progressive depending on the coupling design and material.

The value given for couplings with linear torsional stiffness considers following terms:

- Pre-load: 50% of T_{KN}
- Amplitude of vibratory torque: 25% of T_{KN}
- Ambient temperature: 20°C
- Frequency: 10 Hz

For couplings with progressive torsional stiffness only the pre-load value changes as stated.

The tolerance of the torsional stiffness is $\pm 15\%$ if not stated otherwise.

The following influences need to be considered if the torsional stiffness is required for other operating modes:

- Temperature
Higher temperature reduces the dynamic torsional stiffness.
Temperature factor $St_{C_{Tdyn}}$ has to be taken into consideration in the calculation.
- Frequency of vibration
Higher frequencies increase the torsional stiffness.
By experience the dynamic torsional stiffness is 30% higher than the static stiffness. CENTA keeps record of exact parameters.
- Amplitude of vibratory torque
Higher amplitudes reduce the torsional stiffness, therefore small amplitudes result in higher dynamic stiffness. CENTA keeps record of exact parameters.

8
Relative damping
ψ

The relative damping is the relationship of the damping work to the elastic deformation during a cycle of vibration.

The larger this value [ψ], the lower is the increase of the continuous vibratory torque within or close to resonance.

The tolerance of the relative damping is $\pm 20\%$, if not otherwise stated.

The relative damping is reduced at higher temperatures.

Temperature factor St_{ψ} has to be taken into consideration in the calculation.

The vibration amplitude and frequency only have marginal effect on the relative damping.

9
Speed
[min ⁻¹]

The maximum speed of the coupling element, which may occur occasionally and for a short period (e.g. overspeed).

n_{max} The characteristics of mounted parts may require a reduction of the maximum speed (e.g. outer diameter or material of brake discs).

n_d The maximum permissible speed of highly flexible coupling elements is normally 90% thereof.

10
Permissible axial displacement
[mm]

ΔK_a The continuous permissible axial displacement of the coupling.

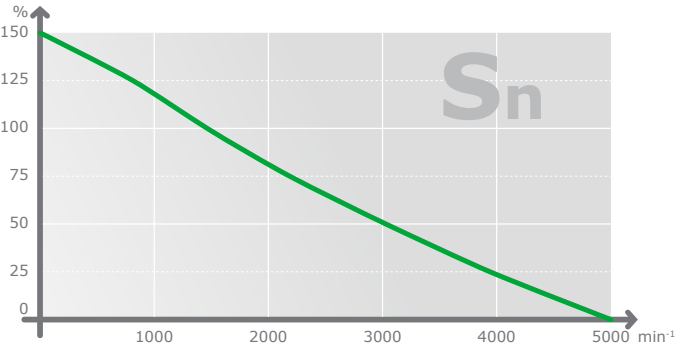
This is the sum of displacement by assembly as well as static and dynamic displacements during operation.

$\Delta K_{a\ max}$ The maximum axial displacement of the coupling, which may occur occasionally for a short period (e.g. extreme load).

The concurrent occurrence of different kinds of displacements is handled in technical documents (displacement diagrams, data sheets, assembly instructions).

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EXPLANATION OF THE TECHNICAL DATA



11	
Axial stiffness [kN/mm]	
C _a	The axial stiffness determines the axial reaction force on the input and output sides upon axial displacement.
C _{a dyn}	By experience the dynamic stiffness is higher than the static one. The factor depends on the coupling series.

12	
Permissible radial displacement [mm]	
ΔK _r	The continuous permissible radial displacement of the coupling. This is the sum of displacement by assembly as well as static and dynamic displacements during operation.
	The continuous permissible radial displacement depends on the operation speed and may require adjustment (see diagrams S _n of the coupling series).
ΔK _{r max}	The maximum radial displacement of the coupling, which may occur occasionally and for a short period without consideration of the operation speed (e.g. extreme overload).
	The concurrent occurrence of different kinds of displacements is handled in technical documents (displacement diagrams, data sheets, assembly instructions).

13	
Radial stiffness [kN/mm]	
C _r	The radial stiffness determines the radial reaction force on the input and output sides upon radial displacement.
C _{rdyn}	By experience the dynamic stiffness is higher than the static one. The factor depends on the coupling series.

14	
Permissible angular displacement [°]	
ΔK _w	The continuous permissible angular displacement of the coupling. This is the sum of displacement by assembly as well as static and dynamic displacements during operation.
	The continuous permissible angular displacement depends on the operation speed and may require adjustment (see diagrams S _n of the coupling series).
ΔK _{w max}	The maximum angular displacement of the coupling, which may occur occasionally and for a short period without consideration of the operation speed (e.g. extreme overload).
	The concurrent occurrence of different kinds of displacements is handled in technical documents (displacement diagrams, data sheets, assembly instructions).

15	
Angular stiffness [kNm/°]	
C _w	The angular stiffness determines the restoring bending moment on the input and output sides upon angular displacement.
C _{w dyn}	By experience the dynamic stiffness is higher than the static one. The factor depends on the coupling series.

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1. This catalog supersedes previous editions.

This catalog shows the extent of our coupling range at the time of printing. This program is still being extended with further sizes and series. Any changes due to technological progress are reserved.

We reserve the right to amend any dimensions or detail specified or illustrated in this publication without notice and without incurring any obligation to provide such modification to such couplings previously delivered. Please ask for an application drawing and current data before making a detailed coupling selection.

2. We would like to draw your attention to the need of preventing accidents or injury. No safety guards are included in our supply.

3. TRADEMARKS

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Other product and company names mentioned herein may be trademarks of their respective companies.

4. Torsional responsibility

The responsibility for ensuring the torsional vibration compatibility of the complete drive train, rests with the final assembler. As a component supplier CENTA is not responsible for such calculations, and cannot accept any liability for gear noise/-damage or coupling damage caused by torsional vibrations.

CENTA recommends that a torsional vibration analysis (TVA) is carried out on the complete drive train prior to start up of the machinery. In general torsional vibration analysis can be undertaken by engine manufacturers, consultants or classification societies. CENTA can assist with such calculations using broad experience in coupling applications and torsional vibration analysis.

5. Copyright to this technical document is held by CENTA Antriebe Kirschey GmbH.

6. The dimensions on the flywheel side of the couplings are based on the specifications given by the purchaser. The responsibility for ensuring dimensional compatibility rests with the assembler of the drive train. CENTA cannot accept liability for interference between the coupling and the flywheel or gearbox or for damage caused by such interference.

7. All technical data in this catalog are according to the metric SI system. All dimensions are in mm. All hub dimensions (N , N_1 and N_2) may vary, depending on the required finished bore. All dimensions for masses (m), inertias (J) and centres of gravity (S) refer to the maximum bore diameter.

CENTA Power Transmission is now part of Rexnord.
As a global leader in premium couplings,
Rexnord provides the same high quality customer
solutions and service you've come to expect
from CENTA since 1970.



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